

# The influence of TIME on my teaching and research

Stephan V Joubert

Tshwane UOT

June 29, 2016

# Pronunciation of names

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- I too have trouble with African names such as
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- My career before TIME
- My career after TIME
- Throughout I will discuss some low cost real-life classroom exercises for under- and post graduates that have pointed me in the direction of some high-level technical publications.
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- **Carsten Schmidt** who taught me to do my teaching in the CAS laboratory whenever possible (I still do this today during my one-day-a-week class).

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- In 1975 I commenced my career at Tshwane University of Technology (TUT), teaching undergraduate physics, moving to the Department of Mathematics and Statistics (DMS) in 1981 and retiring there as “Professor Emeritus” in 2014 (**40 years of service and still keeping my hand in**).
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- My colleagues mostly had four-year bachelor's degrees (or an equivalent degree) and so a research environment in the DMS was almost non-existent.
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- In 1997, as a first step towards doing some research in applied mathematics I **advertised my willingness to help any colleagues** who needed mathematical modeling for their own research.
- I was soon approached to give a series of lectures as part of an undergraduate course in explosive technology where I rubbed shoulders with a colleague (in the Department of Explosives Technology) doing her masters degree.
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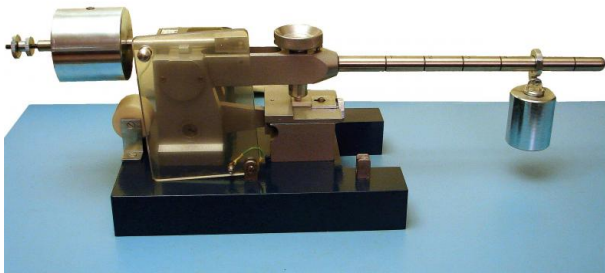
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- A small amount of explosive is spread onto the rough surface of the tile and a blunt pin is dragged across the rough surface. The amount of force needed to ignite the explosive can be varied as illustrated above.

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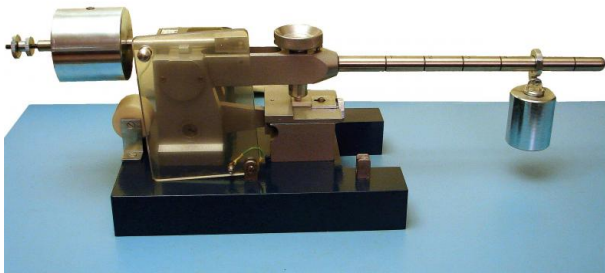


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- Then, using a drill bit of radius say  $r = 180 \mu m$ , she produced parallel grooves on one surface before baking the tiles.

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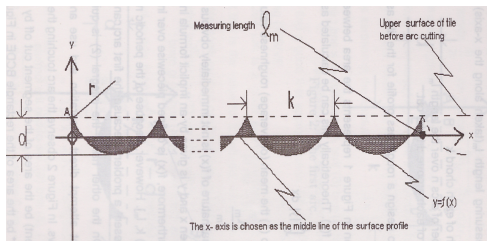
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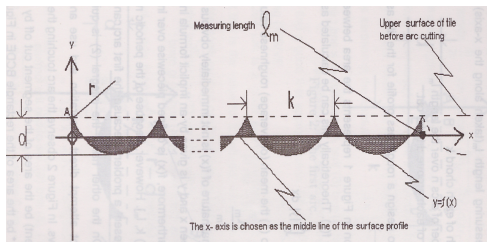
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# Design of ceramic tiles (continued)

- The function  $f(x)$  models the surface displacement above the  $x$ -axis.



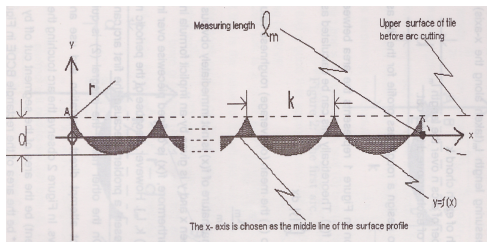
- The **arithmetic mean roughness value** (ISO/DIS 4768/1) of a surface is defined as

$$R_a = \frac{\int_0^{l_m} |f(x)| dx}{l_m}$$

where  $l_m$  is the so-called measuring length.

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# Design of ceramic tiles (continued)

- Prescribing that  $r = 180 \mu\text{m}$  and  $R_a = 18.5 \mu\text{m}$  and solving a transcendental equation using DERIVE yielded

$$k = 263.9 \mu\text{m}.$$

```
#12: ITERATES k -  $\frac{\frac{1}{2} 180^2 \left[ 2 \operatorname{ASIN}\left[\frac{k}{2 180}\right] - \operatorname{SIN}\left[2 \operatorname{ASIN}\left[\frac{k}{2 180}\right]\right] \right]}{\frac{d}{dk} \left[ \frac{1}{2} 180^2 \left[ 2 \operatorname{ASIN}\left[\frac{k}{2 180}\right] - \operatorname{SIN}\left[2 \operatorname{ASIN}\left[\frac{k}{2 180}\right]\right] \right] - k 18.5}$ 
#13: [264, 263.003, 263.002, 263.002, 263.002, 263.002, 263.002]
COMMAND: Author Build Calculus Declare Expand Factor Help Jump solve Manage
Options Plot Quit Remove Simplify Transfer Unremove solve Window approx
Enter option
Approx(#12) C:\DERIVE3.05\CERAM Free:04% Derive Algebra
```

- With  $\ell_m = 800 \mu\text{m}$  the number of grooves to cut was

$$n = 3$$

to a depth of

$$d = 58 \mu\text{m}.$$



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The screenshot shows the DERIVE software interface. It displays the iterative solution of a transcendental equation for  $k$ . The equation is:

$$\frac{1}{2} \cdot 180^2 \left[ 2 \operatorname{ASIN}\left[\frac{k}{2 \cdot 180}\right] - \operatorname{SIN}\left[2 \operatorname{ASIN}\left[\frac{k}{2 \cdot 180}\right]\right] \right] - k \cdot 18.5$$

The software shows the result of the iteration as  $k = 263.902$ . The command window shows the following text:

```
COMMAND: Author Build Calculus Declare Expand Factor Help Jump solve Manage
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Approx(#12) C:\DERIVE3.05\CERAM Free:84% Derive Algebra
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  - twelve doctoral and
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- **Equipment needed:**

- Plastic soccer ball
- Kitchen or chemical scale
- Bathroom scale
- Ruler
- Measuring tape or metre rule
- Any CAS

- Typically our students have two semesters of calculus before they register for an introductory ODE course.
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# The bouncing soccer ball

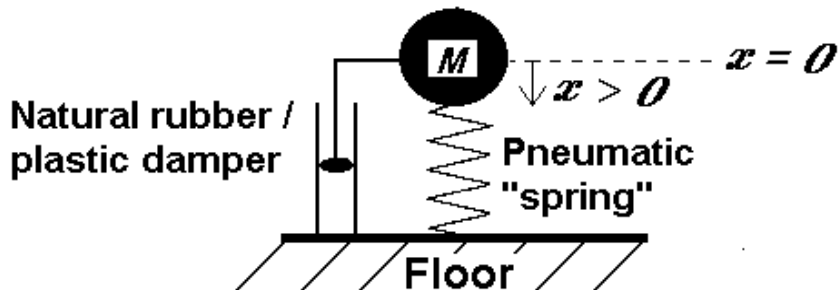
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## The bouncing soccer ball (continued)

- The ODE to consider solving for the simplified model of one bounce is

$$M\ddot{x} + B\dot{x} + Kx = 0$$

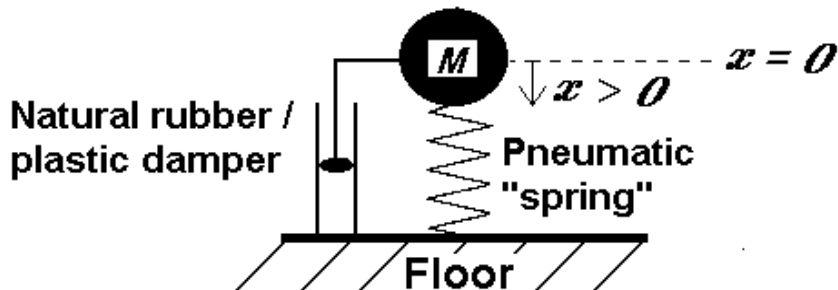


- A **kitchen scale** is used to measure the mass of the ball  $M$ .
- To measure the spring constant  $K$ , place the ball on top of a **bathroom scale**.
  - Push down and hold the position at say a reading of 20 kg on the scale.
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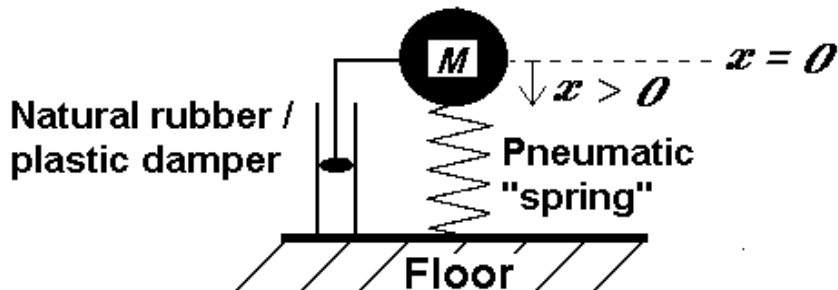
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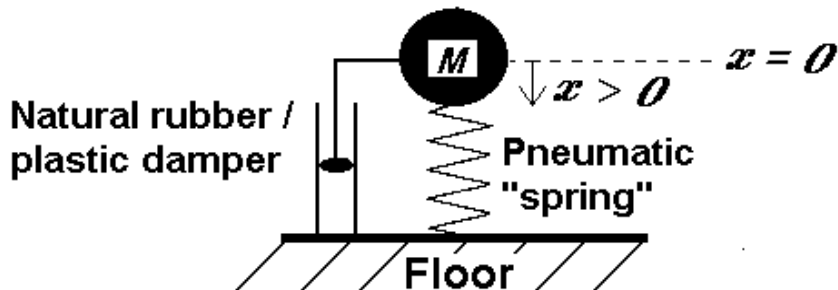


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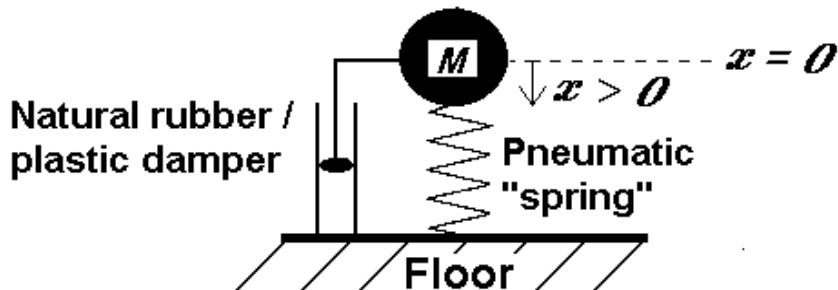


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# The bouncing soccer ball (continued)



- We found the compression distance to be approximately  $\Delta x = 6 \text{ cm}$ .
- From Hooke's law the ball "spring constant"  $k$  may be obtained.

$$K = \frac{Mg}{\Delta x}$$
$$K = \frac{20 \times 9.8}{0.06}$$
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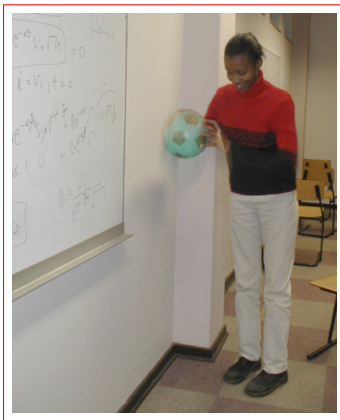
# The bouncing soccer ball (continued)

- Determining the damping coefficient  $B$  of the rubber ball is more difficult. One cannot pull on the ball as one would on a shock absorber.



# The bouncing soccer ball (continued)

- With a little mathematical "trickery" one can use the **coefficient of restitution** of the ball instead, by measuring the height of drop  $h_1$  and the height of bounce  $h_2$  using a **tape measure**.





# Coefficient of restitution

- The coefficient of restitution  $R$  of the ball is the ratio of the incident velocity before bounce to the reflection velocity after bounce.
- The high school formula

$$v^2 = 2gh$$

is used to show that

- 

$$R = \sqrt{\frac{h_2}{h_1}}$$
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- Applying these measurements to the equation of motion of the ball considered as a spring-damper pair, the trajectory of the ball may be modelled mathematically using DERIVE or any suitable CAS.

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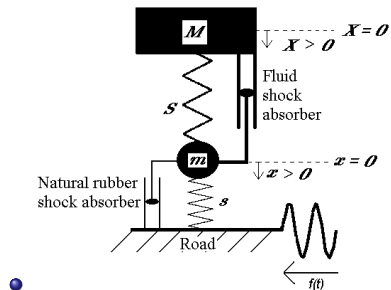
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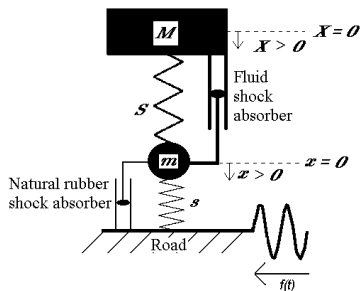
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# New Zealand DELTA03: An affordable, realistic student model of a motor-vehicle suspension system



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# Motor-vehicle suspension system



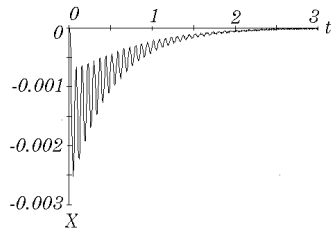
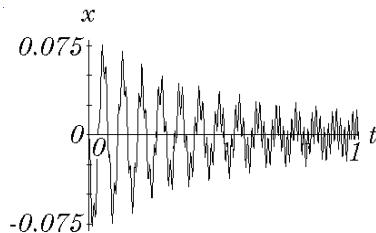
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# Motor-vehicle suspension system

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- I had our team (Temple Fay, Keith Hardie, Anton van Wyk, Ansie Greeff et cetera) thinking about bouncing soccer balls and vehicle suspension systems.
- While driving over a corrugated dirt road in the Pilansberg Game Reserve near Pretoria (close to Buffelspoort where TIME2008 was held), I asked "I wonder how corrugations form". Keith went quiet for a while and then announced "I think I know how".
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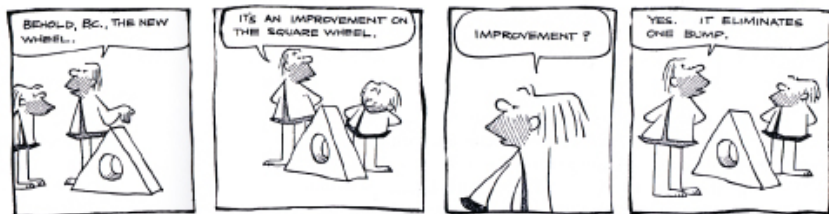
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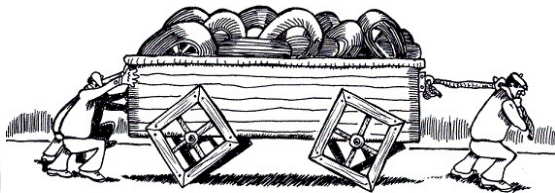
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By permission of Johnny Hart and Field Enterprises, Inc.

# Wheel (continued)

- Stan Wagon improved on BC's wheel by making a square wheel bicycle that rides smoothly over a catenary road:





## Wheel (continued)

- **Seriously**, our patent outlines the design of a wheel with a tyre that resists the formation of dirt road corrugations by **reducing the tangential vibrations of the surface of the tyre** on the road. Our contention is that **it is the tangential vibrations** of the tyre and **not the radial vibrations** of the tyre and vehicle springs **that cause corrugations**.

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- **Human resource development:**
  - I supervised, with Temple Fay, the masters (USM) and doctoral (TUT) studies of Dr. Annatjie Bekker our colleague from the Central UOT in South Africa. Annatjie's thesis dealt with dirt road corrugations and provided evidence to support our patent wheel design.

- **Seriously**, our patent outlines the design of a wheel with a tyre that resists the formation of dirt road corrugations by **reducing the tangential vibrations of the surface of the tyre** on the road. Our contention is that **it is the tangential vibrations** of the tyre and **not the radial vibrations** of the tyre and vehicle springs **that cause corrugations**.
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  - Indeed, she found among other results that corrugations have a wavelength of about 40 cm and that the frequency of vibrations (about 42 Hz) of a vehicle travelling at  $60 \text{ km h}^{-1}$  agrees well with the frequency (about 44 Hz) of tangential vibrations of a rubber tyre while radial spring frequency (about 2 Hz) vibrations are not even of the same order of magnitude as tangential vibrations.

# Visit-Me TIME, Vienna, 2002: Dimension Analyses (with Temple Fay)

- Dimension analyses (DA) is folklore, but DA that results in a system of say three simultaneous equations with five unknowns is not readily understood by undergraduates at a UOT.
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$$T \approx 2\pi \sqrt{\frac{\ell}{g}}.$$

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# Dimension Analyses

- In order to derive this result using DA, we form the dimensionless product

$$\Pi_{Gen} = T^{x_1} \times \theta_0^{x_2} \times \ell^{x_3} \times M^{x_4} \times g^{x_5}.$$

- Hence we obtain the system of linear equations:

$$m : 0x_1 + 0x_2 + x_3 + 0x_4 + x_5 = 0$$

$$kg : 0x_1 + 0x_2 + 0x_3 + x_4 + 0x_5 = 0$$

$$s : x_1 + 0x_2 + 0x_3 + 0x_4 - 2x_5 = 0$$

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- Hence we see that  $x_4 = 0$  and so mass does not play a role! It is obvious that we have two fundamental solutions:

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$$T = \frac{\Psi(\theta_0)}{\left(\frac{g}{l}\right)^{1/2}} = \Psi(\theta_0) \times \sqrt{\frac{l}{g}}$$

- where  $\Psi$  is a function of  $\theta_0$ . An experiment can be conducted using small oscillations that shows that

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# Testing Accuracy of RK4

- Turn this IVP into a  $2 \times 2$  system IVP as follows

$$\begin{aligned}\dot{x} &= y \\ \dot{y} &= 2y + 3x - 4e^t \\ x(0) = 2, \quad y(0) &= 0.\end{aligned}$$

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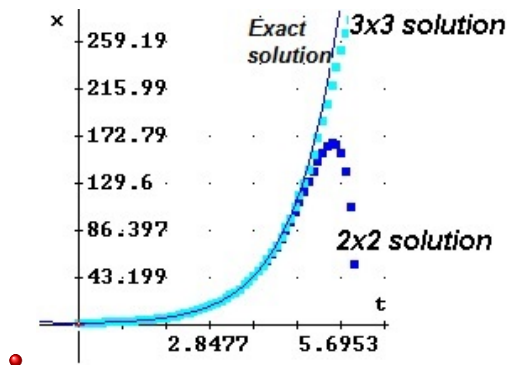
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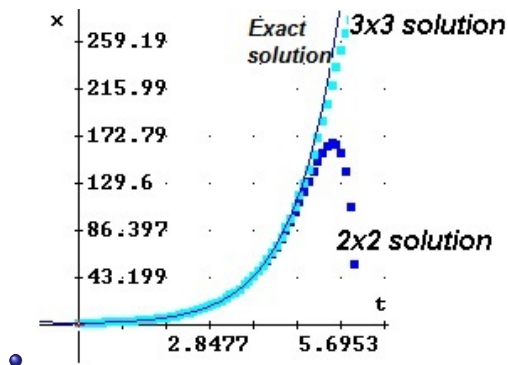


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<i>t</i>	<i>Actual Error</i>	<i>t</i>	<i>Estimated Error</i>
1	$9.061932091 \cdot 10^{-5}$	1	$-5.943768169 \cdot 10^{-5}$
1.1	0.0001261640890	1.1	$-8.297205588 \cdot 10^{-5}$
1.2	0.0001745509993	1.2	$-0.0001150529184$
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1.6	0.0006145616139	1.6	$-0.0004075046692$
1.7	0.0008365435693	1.7	$-0.0005552157854$
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- **Professor Dr. Ansie Greeff**, my colleague and my doctoral student, has become well known in the field of mathematical biology. She has, with Temple Fay, developed a three competing species model with and without cropping.
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- **Equipment needed:**

- The qualitative effect of an earthquake or tornado moving down the edge of a bay or harbour can be observed in a classroom, with minimal apparatus.
- Indeed, anyone who causes a partially filled wineglass to "sing" (resonate) using a wet finger can observe the effect.
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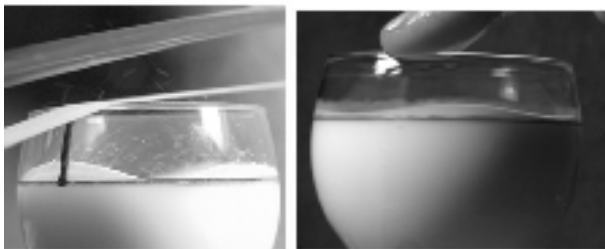
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# Singing wineglass

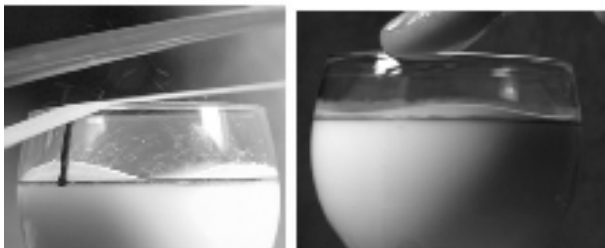
- Clearly the anti-node is below the energy source (the violin bow) when the glass is not rotating:



- The photograph on the left depicts a clockwise rotating glass and a static energy source (the finger).
- The Coriolis forces involved cause the anti-node to move to a fixed position away from the finger in the opposite direction to the rotation.
- In 1890 GH Bryan observed that he could not hear four beats when he turned a ringing wineglass through  $360^\circ$ .

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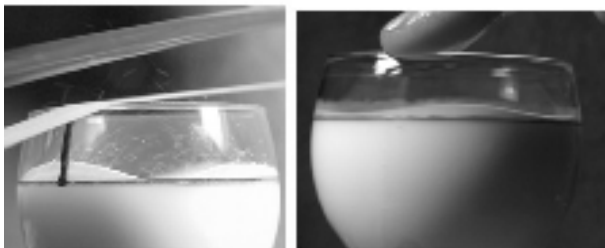
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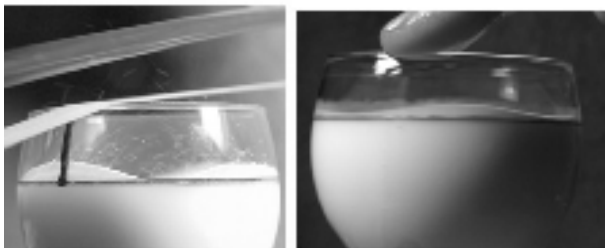
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"When a vibrating body rotates, the rotation pattern rotates away from its position of rest at a rate **proportional** to the rotation rate of the body".
- Indeed, **Bryan's factor** is the constant

$$\eta = \frac{\text{Angular rate of the vibrating pattern}}{\text{Angular rate of the vibrating body}}$$

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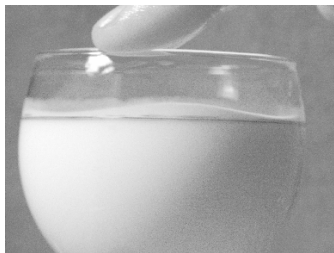
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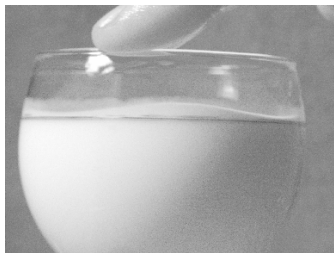
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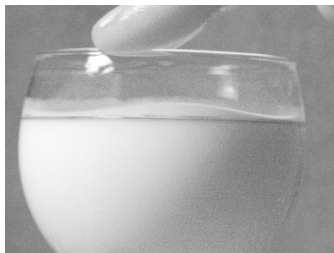
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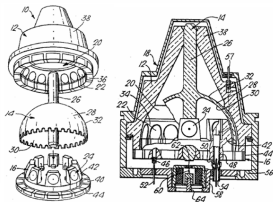
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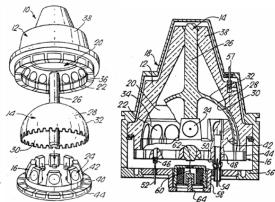
U.S. Patent Aug. 28, 1990 Sheet 1 of 12 4,951,508



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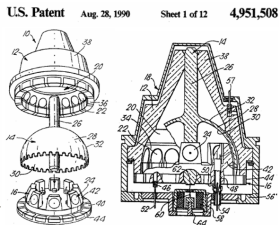
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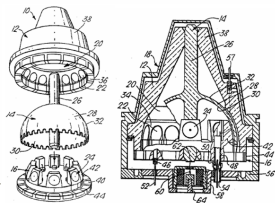




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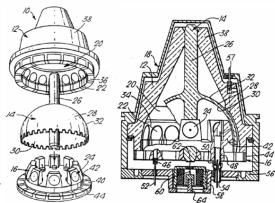
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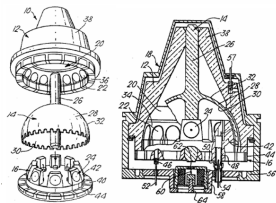
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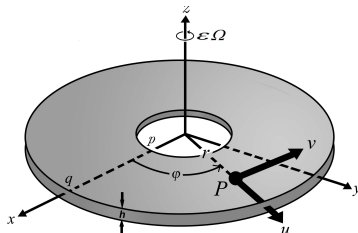
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# Malaga-TIME 2010, Spain: A CAS routine for obtaining eigenfunctions for Bryan's effect

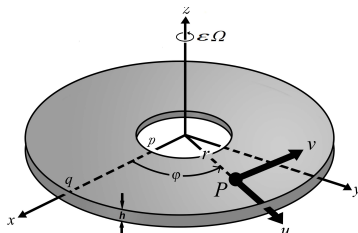
- Consider a vibrating, slowly rotating annular disc:



- The polar coordinates  $r$  and  $\varphi$  of the position of rest  $P$  of a vibrating particle in the annular disc of density  $\rho$ , height  $h$ , rotating slowly at rate  $\varepsilon\Omega$ . The vibrating particle at  $P$  has **radial** displacement  $u$  and **tangential** displacement  $v$

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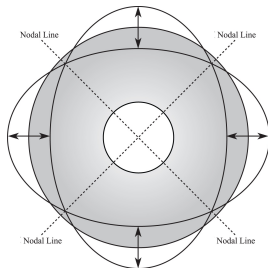
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where,  $C(t)$  and  $S(t)$  are to be determined and  $m$  is the circumferential wave number.

- It has been demonstrated that  $\omega^2 = \frac{2 \int_p^q UVrdr}{\int_p^q (U^2 + V^2)rdr} = \frac{l_2}{l_0}$ .

- When  $m = 2$  the vibration pattern has four nodes:



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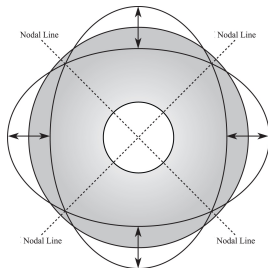
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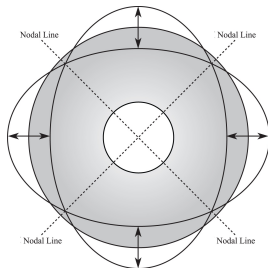
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- Applying Newton's laws of motion to the mass element at point  $P$ , one arrives at two coupled PDE, and, assuming harmonic solutions, we arrive at a system of two coupled *linear, ordinary differential equations* (ODEs)

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- where, with  $\rho$  mass density,  $E$  Young's modulus and  $\mu$  Poisson's ratio we have

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# Iteration process

- For a given substance and circumferential wave number  $m$ , the constants  $a, b, c, d, e$  are known. If a value is assigned to  $\omega$ , then the NDSolve routine of Mathematica will produce a numerical solution for suitable boundary conditions.
- For a **guess value** of  $\omega$ , MATHEMATICA® stores  $U$  and  $V$  as **interpolating functions**. A new value for  $\omega$  may now be generated by MATHEMATICA® via the known formula

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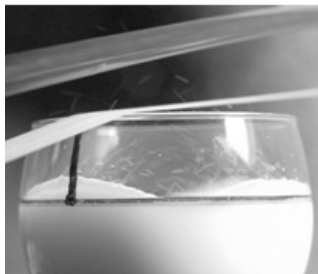
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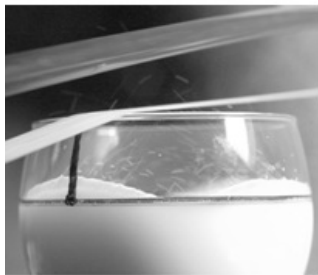
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- Recall that we set

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- Notice that, for instance

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- If we consider the density as a Fourier Series

$$\rho(\varphi) = \rho_0(1 + \varepsilon \sum_{k=1}^{\infty} (a_k \cos k\varphi + b_k \sin k\varphi))$$

- Then only the zeroth and  $2m^{\text{th}}$  harmonics play a roll in the kinetic energy expression and so we might as well choose

$$\rho(\varphi) := \rho_0 \left[ 1 + \varepsilon \frac{4l_0}{l_3} (\rho_c \cos 2m\varphi + \rho_s \sin 2m\varphi) \right].$$

- where for simplification purposes, we have set  $a_{2m} = 4 \frac{l_0}{l_3} \rho_c$  and  $b_{2m} = 4 \frac{l_0}{l_3} \rho_s$  with  $\rho_c$  and  $\rho_s$  dimensionless constants that we will call the coefficients of the  $2m^{\text{th}}$  harmonics. The ratio  $\frac{l_0}{l_3}$  is a ratio of definite integrals (we have already seen something similar with

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$$\text{In[128]:= FullSimplify}\left[\frac{\rho_0 h}{2} \left(4 \epsilon \frac{I_0}{I_3} \rho_c\right) \int_0^{2\pi} \int_p^q \cos[2 m \varphi] \left((\partial_t u[x, \varphi, t])^2 + (\partial_t v[x, \varphi, t])^2\right) r dr d\varphi, m \in \text{Integers}\right]$$

$$\text{Out[128]:= } \left\{ \frac{1}{I_3} 2 h \epsilon \left( \int_p^q \frac{1}{2} \pi r (U[r]^2 - V[r]^2) (C'[t]^2 - S'[t]^2) dr \right) I_0 \rho_0 \rho_c \right\}$$

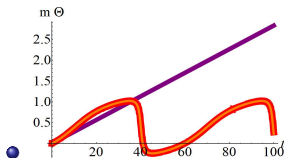
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# Capture effect

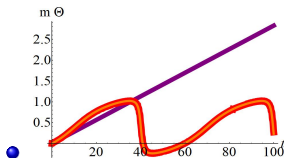
- Considering the vibration pattern for the  $m^{\text{th}}$  circumferential wave number  $m\Theta$ , we have chosen ODE coefficients that show the following **capture effect**:



- The purple line indicates the ideal case with the precession angle  $m\Theta$  for a slowly rotating disk changing linearly while the precession angle for a slowly rotating disk with light mass imperfections is "captured" periodically (the red/orange curve).
- Spin-off publication**
  - Article published in 2014 in the **Journal of Symbolic Computation (TIME 2012 Proceedings)**: "Using Fourier series to analyse mass imperfections in vibratory gyroscopes" with Michael Shatalov and Charlotta Coetzee.

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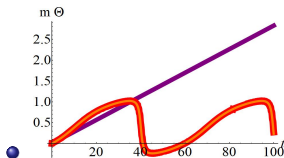
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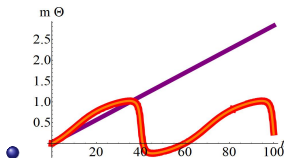


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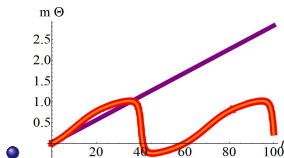
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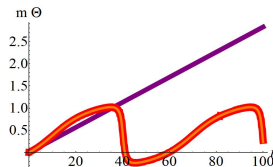
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Recall the graph of the "capture effect" caused by mass (and possibly other) imperfections.



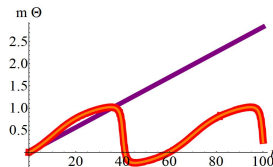
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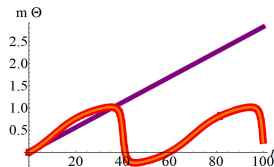
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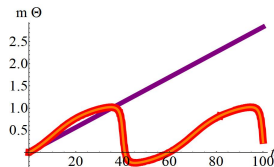
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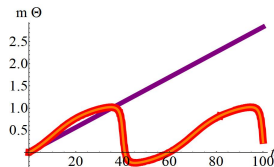
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- Mass imperfections cause **beats** (that can be heard in large VGs). Indeed, we have shown that the frequency of the beats is given by

$$f = \frac{\varepsilon\omega\sqrt{\rho_c^2 + \rho_s^2}}{2\pi}$$

where the coefficients of the  $2m^{\text{th}}$  harmonics come from the Fourier series for the density

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# Equations of motion

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- Indeed, those of an ideal annular VG are

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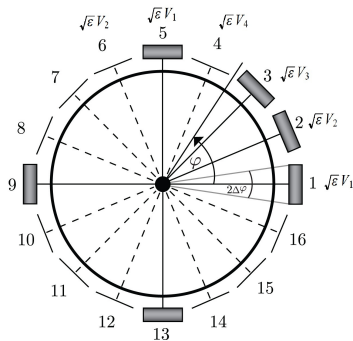
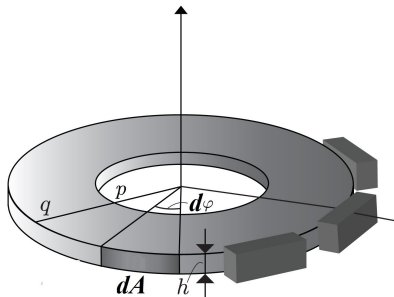
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# Capacitor array

- Observe an annulus of thickness  $h$  surrounded by an array of electronic plates each at a small distance  $d$  from the cylindrical surface of the annulus. These plates, together with the cylindrical surface of the annulus approximate a "parallel plate capacitor" array:



# Small potential differences

- Assume that small potential differences  $\sqrt{\varepsilon}V_1$ ,  $\sqrt{\varepsilon}V_2$ ,  $\sqrt{\varepsilon}V_3$  and  $\sqrt{\varepsilon}V_4$  are maintained between the plate and the disc for capacitors numbered one to four respectively, where we use the small parameter  $\varepsilon$  again to emphasise smallness.
- Assume that the other potential difference around the disc are  $\frac{\pi}{2}$  periodic in the sense that capacitor number five has potential difference  $\sqrt{\varepsilon}V_1$ , capacitor number six has potential difference  $\sqrt{\varepsilon}V_2$ , et cetera.
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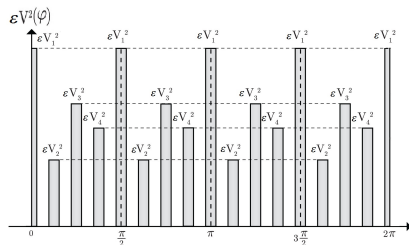
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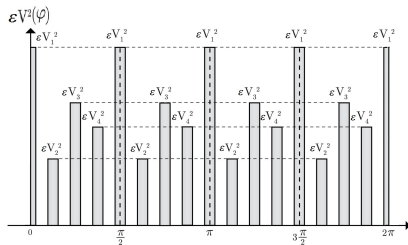
# Fourier series



- Because of the periodicity involved with the potentials, we may determine a Fourier series for the function  $V^2(\varphi)$  depicted in the figure as follows

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# Fourier coefficients

We use MATHEMATICA<sup>®</sup> to determine the  $a_n$  and  $b_n$ :

In[6]:=  $a_n :=$

$$\frac{1}{\pi} \text{FullSimplify} \left[ \int_0^{\Delta\varphi} \varepsilon V_1^2 \cos[n\varphi] d\varphi + \int_{\frac{\pi}{8}-\Delta\varphi}^{\frac{\pi}{8}+\Delta\varphi} \varepsilon V_2^2 \cos[n\varphi] d\varphi + \int_{\frac{\pi}{4}-\Delta\varphi}^{\frac{\pi}{4}+\Delta\varphi} \varepsilon V_3^2 \cos[n\varphi] d\varphi + \right. \\ \left. \int_{\frac{3\pi}{8}-\Delta\varphi}^{\frac{3\pi}{8}+\Delta\varphi} \varepsilon V_4^2 \cos[n\varphi] d\varphi + \int_{\frac{\pi}{2}-\Delta\varphi}^{\frac{\pi}{2}+\Delta\varphi} \varepsilon V_1^2 \cos[n\varphi] d\varphi + \int_{\frac{5\pi}{8}-\Delta\varphi}^{\frac{5\pi}{8}+\Delta\varphi} \varepsilon V_2^2 \cos[n\varphi] d\varphi + \int_{\frac{3\pi}{4}-\Delta\varphi}^{\frac{3\pi}{4}+\Delta\varphi} \varepsilon V_3^2 \cos[n\varphi] d\varphi + \right. \\ \left. \int_{\frac{7\pi}{8}-\Delta\varphi}^{\frac{7\pi}{8}+\Delta\varphi} \varepsilon V_4^2 \cos[n\varphi] d\varphi + \int_{\pi-\Delta\varphi}^{\pi+\Delta\varphi} \varepsilon V_1^2 \cos[n\varphi] d\varphi + \int_{\frac{9\pi}{8}-\Delta\varphi}^{\frac{9\pi}{8}+\Delta\varphi} \varepsilon V_2^2 \cos[n\varphi] d\varphi + \int_{\frac{5\pi}{4}-\Delta\varphi}^{\frac{5\pi}{4}+\Delta\varphi} \varepsilon V_3^2 \cos[n\varphi] d\varphi + \right. \\ \left. \int_{\frac{11\pi}{8}-\Delta\varphi}^{\frac{11\pi}{8}+\Delta\varphi} \varepsilon V_4^2 \cos[n\varphi] d\varphi + \int_{\frac{3\pi}{2}-\Delta\varphi}^{\frac{3\pi}{2}+\Delta\varphi} \varepsilon V_1^2 \cos[n\varphi] d\varphi + \int_{\frac{13\pi}{8}-\Delta\varphi}^{\frac{13\pi}{8}+\Delta\varphi} \varepsilon V_2^2 \cos[n\varphi] d\varphi + \right. \\ \left. \int_{\frac{7\pi}{4}-\Delta\varphi}^{\frac{7\pi}{4}+\Delta\varphi} \varepsilon V_3^2 \cos[n\varphi] d\varphi + \int_{\frac{15\pi}{8}-\Delta\varphi}^{\frac{15\pi}{8}+\Delta\varphi} \varepsilon V_4^2 \cos[n\varphi] d\varphi + \int_{2\pi-\Delta\varphi}^{2\pi} \varepsilon V_1^2 \cos[n\varphi] d\varphi \right]$$

Table[ $a_n$ , { $n$ , 0, 14}]

$$\text{Out[7]} = \left\{ \frac{8 \Delta\varphi \varepsilon (V_1^2 + V_2^2 + V_3^2 + V_4^2)}{\pi}, 0, 0, 0, \frac{2 \varepsilon \sin[4 \Delta\varphi] (V_1^2 - V_3^2)}{\pi}, 0, 0, \right. \\ \left. 0, \frac{\varepsilon \sin[8 \Delta\varphi] (V_1^2 - V_2^2 + V_3^2 - V_4^2)}{\pi}, 0, 0, 0, \frac{2 \varepsilon \sin[12 \Delta\varphi] (V_1^2 - V_3^2)}{2 \pi}, 0, 0 \right\}$$

In[8]:= Table[ $b_n$ , { $n$ , 1, 14}]

$$\text{Out[8]} = \left\{ 0, 0, 0, \frac{2 \varepsilon \sin[4 \Delta\varphi] (V_2^2 - V_4^2)}{\pi}, 0, 0, 0, 0, 0, 0, 0, \frac{2 \varepsilon \sin[12 \Delta\varphi] (-V_2^2 + V_4^2)}{3 \pi}, 0, 0 \right\}$$

# Equations of motion

- Recall that  $\omega^2 = \frac{l_2}{l_0} = \frac{2 \int_p^q UV_r dr}{\int_p^q (U^2 + V^2)_r dr}$  and examine the equations of motion that include mass imperfections and electrical potentials:



$$\begin{pmatrix} \ddot{C} \\ \ddot{S} \end{pmatrix} + \frac{1}{l_0} \begin{pmatrix} l_2 - \varepsilon k_1 - \varepsilon [k_2 + \rho_c l_2] & -\varepsilon [k_3 + \rho_s l_2] \\ -\varepsilon [k_3 + \rho_s l_2] & l_2 - \varepsilon k_1 + \varepsilon [k_2 + \rho_c l_2] \end{pmatrix} \begin{pmatrix} C \\ S \end{pmatrix} = 2\eta\varepsilon\Omega \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \begin{pmatrix} \dot{C} \\ \dot{S} \end{pmatrix}$$

- where

$$k_1 = \frac{4\Delta\phi hq\varepsilon_0 U^2(q)}{\pi d^3} (V_1^2 + V_2^2 + V_3^2 + V_4^2)$$

$$k_2 = \frac{hq\varepsilon_0 \sin(4\Delta\phi) U^2(q)}{\pi d^3} (V_1^2 - V_3^2)$$

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# Negating mass imperfection

- Because  $k_2 \propto (V_1^2 - V_3^2)$  and  $k_3 \propto (V_2^2 - V_4^2)$ , if we arrange capacitor voltage so that

$$\varepsilon[k_2 + \rho_c l_2] = 0 \quad \& \quad \varepsilon[k_3 + \rho_c l_3] = 0,$$

- then the equations of motion reduce to

$$\begin{pmatrix} \ddot{C} \\ \ddot{S} \end{pmatrix} + \frac{l_2 - \varepsilon k_1}{I_0} \begin{pmatrix} C \\ S \end{pmatrix} = 2\eta\varepsilon\Omega \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \begin{pmatrix} \dot{C} \\ \dot{S} \end{pmatrix}.$$

- Compare this with the equations of motion of an *ideal annular gyroscope*:

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# Negative stiffness

- Hence, the capacitors have produced a gyroscope with mass imperfections that behaves "ideally" and is vibrating with a slightly reduced angular rate

$$\omega^* = \sqrt{\frac{I_2 - \varepsilon k_1}{I_0}}$$

where  $-\varepsilon k_1$  reduces the stiffness integral  $I_2$  and is called **negative stiffness**. The term  $-\varepsilon k_1$  will never disappear because  $k_1 \propto (V_1^2 + V_2^2 + V_3^2 + V_4^2)$ .

- An annular vibratory gyroscope manufactured by including this array of capacitors and manipulating them appropriately will be able to utilise Bryan's factor  $\eta$  to determine the rotation rate  $\varepsilon\Omega$  of the vehicle in which it is mounted using the formula

$$\varepsilon\Omega = \frac{\text{Rate of rotation of the vibrating pattern of the gyroscope}}{\eta}$$

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